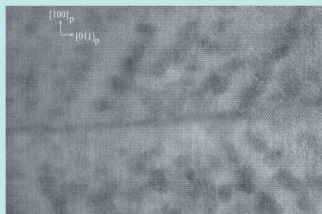
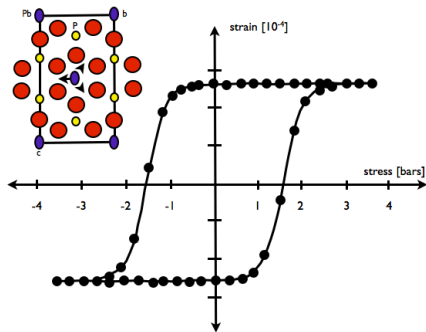
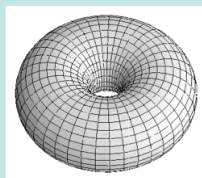
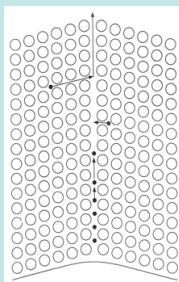


*Domain boundary engineering in
(multi-) ferroics
-concepts-*

*Ekhard Salje
University of Cambridge*



Typical wall thickness in perovskites at $T \ll T_c$ is $> 2\text{nm}$



flexoelasticity: with a twin angle is 4° it would correspond to 90 segments in a torus with 2nm wall width and 60 nm diameter if all twin angles would be in the same direction with no domains in between (in fact they are zig-zag): all flexo-effects are hence high in twin walls (transport, band structure deformations, photovoltaics, multiferroics etc)!

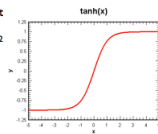
The bulk: How to construct a Landau potential

Double well potential and order parameters
 $G(Q) = 1/2 A Q^2 + 1/4 B Q^4 + 1/6 C Q^6 + 1/2 g (\text{grad}_x Q)^2$
 coupling $(-eQ - PQ - MQ \dots)$ leads to
 $G(Q, T, P, e, \mu, H, \dots)$
 relaxation of G ($\partial G / \partial e = 0, \partial G / \partial \mu = 0, \partial G / \partial m = 0$)
 leads to and equilibrium G with field
 $G(Q, T, P, H, \dots)$
 and field - free $\sigma = E = H = 0$
 $G(Q, T, P, e, \mu, H, \dots)$

DFT and other simulations can be put into the Landau framework: Landau theory is the playground where theory (of any kind) and experiment can meet.

Landau Ginzburg potential and the Euler-Lagrange equation

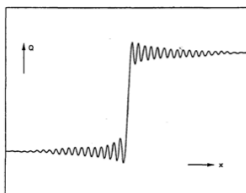
- Landau + dispersion term = Landau Ginzburg potent
- $G(Q) = 1/2 A Q^2 + 1/4 B Q^4 + 1/6 C Q^6 + 1/2 g (\text{grad}_x Q)^2$
- minimization: $\min G(Q)$ with boundary conditions,
- klink: $Q_0 = 1$ for $x \rightarrow \infty$ and $Q_0 = -1$ for $x \rightarrow -\infty$
- $\partial^2 Q / \partial x^2 = 1/g (A Q + B Q^3 + C Q^5)$
- most Euler-Lagrange equ. have NO analytical solution BUT for $C=0$ one finds the most important solution: $Q = Q_0 \tanh(x/w)$ with $w = (2g/A)^{1/2}$
- numerical solutions can be found easily, in perturbation theory one can write $Q = Q_0 \tanh(x/w) + \epsilon(Q)$



Ripple states

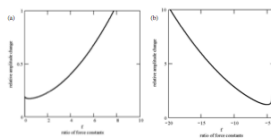
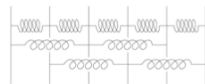
solution can become unstable so that higher order terms become necessary:
 $+ 1/2 d Q^2 (\nabla Q)^2 + 1/2 (\Delta Q)^2$

- trial function $Q = p + q \sin kx$ leading to
 $G = A p^2 + 1/2 p^4 + 1/2 A q^2 + 3/2 p^2 q^2 + 3/16 q^4 + (-\gamma/2 q^2 + d p^2 q^2 + d/4 q^4) k^2 + 1/2 q^2 k^4$
- stable k vector : $k^2 = 1/2 \gamma - d(p^2 + 1/4 q^2) > 0$
- $32G = -d^2 q^4 + (6+47\gamma d) q^4 - (16+4\gamma^2) q^2 + 16 p^4 + 32 A p^2 - 8 d^2 p^2 q^2 (2 p^2 + q^2) + (48 + 16\gamma d) p^2 q^2$.

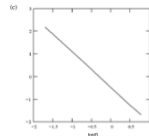


Ripple states near twin boundaries and surfaces

Mechanical model



(a) Pressure dependence of the relative change of the relaxation amplitude in the 'anti-ferroelastic' regime ($\lambda > 0$). No singularity occurs for uniform stress fields. (b) Pressure dependence of the relative change of the relaxation amplitude in the 'ferroelastic' regime ($\lambda < 0$). Note the singularity at the $f = -4$ transition point. (c) Log/log plot of the pressure amplitude multiplied by the characteristic volume ($\log(\epsilon_0 / \ln \lambda)$) versus the ratio of the force constants



The two-spring model with free surfaces. Nearest neighbour layers are connected by a spring with force constant ϕ_1 , the second nearest neighbours are connected by springs with the force constant ϕ_2 ($f = \phi_1 / \phi_2$). The equilibrium distances are a_1 and a_2 , the misfit parameter is $2a_1 - a_2$.

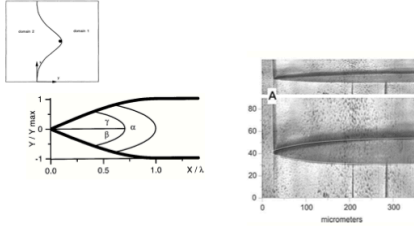
$H = \Sigma (\phi_1 / 2 (b + \epsilon_1 - a_1)^2 + \phi_2 / 2 (2b + \epsilon_1 + \epsilon_{i+1} - a_2)^2)$
 relaxation has a length scale: $\lambda = \pm 1/2 (f^2 + 4f)^{1/2} - 1/2f - 1$

wall orientation, analytical and by simulation

condition for strain walls to align along the 'easy' directions is that the strain tensors on both sides are rank 1 connected, explicitly for vanishing volume strain the compatibility relation:

$$[e_{ik}(S_1) - e_{ik}(S_2)] x_i x_k = 0$$

conditions for wall-bending is then that the compatibility=anisotropy energy $E_{\text{anisotropy}} = U(dy/dx)^2$ and the wall bending energy $E_{\text{bending}} = S(d^2y/dx^2)^2$ are minimised:



The hamiltonian

elastic forces are long-ranging:

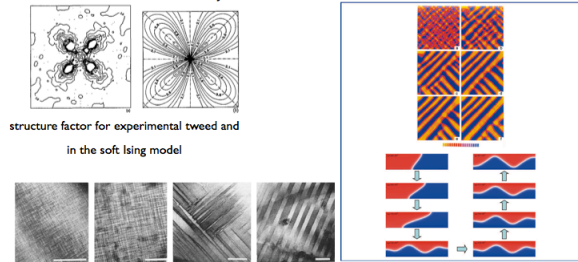
ferro: $J(R) \sim (A_2 Y_{2m} + A_4 Y_{4m}) / R^3 + Jz$

antiferro: $J(R) \sim (A_2 Y_{2m} + A_4 Y_{4m}) / R^5$

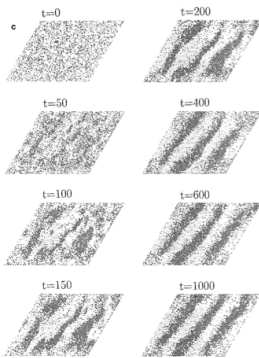
bilinear coupling with the ordering scheme leads to a soft Ising model

$$J_k = C_{\alpha\beta\gamma\lambda} \epsilon_{\alpha\beta} \epsilon_{\gamma\lambda} \cdot P \text{ for } k=0$$

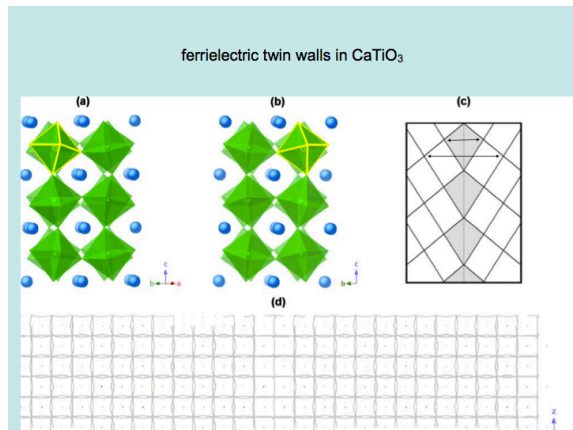
$$J_k = F_k^{\alpha} G_{\alpha\beta} F_k^{\beta} \cdot P \text{ for } k \neq 0$$



structure factor for experimental tweed and in the soft Ising model



computer simulation of the annealing of a feldspar structure with Si/Al ordering after deep quench, note the 'easy' strain orientation.



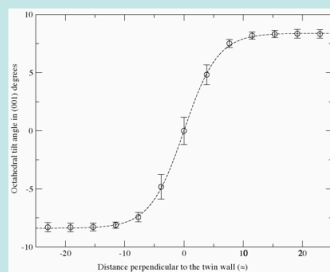
empirical potentials:

$$V(r) = A_{ij} \exp(-b_{ij}r) - C_{ij} / r^6 + q_i q_j / 4\pi\epsilon_0 r$$

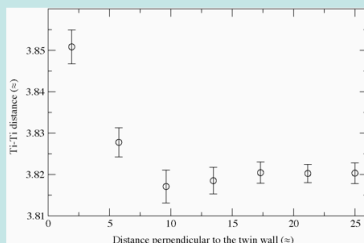
Interaction	A_{ij} (eV)	b_{ij} (\AA^{-1})	C_{ij} (eV \AA^6)	Charge q
O-O	22764.0	6.7114	27.88	$q_{\text{O}} = -2$
Ti-O	3242.124	3.4626	0.0	$q_{\text{Ti}} = 4$
Ca-O	2272.741	3.3490	0.0	$q_{\text{Ca}} = 2$

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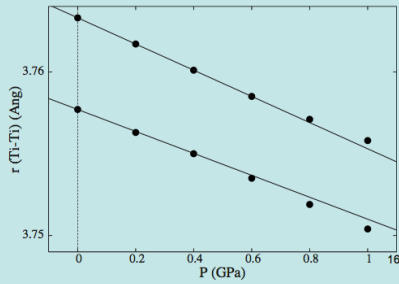
Profile of the primary order parameter (octahedra rotation) in CaTiO₃



Profile of a secondary order parameter in CaTiO₃:
Ti-Ti distances perpendicular to the wall. The wall is positioned at the origin

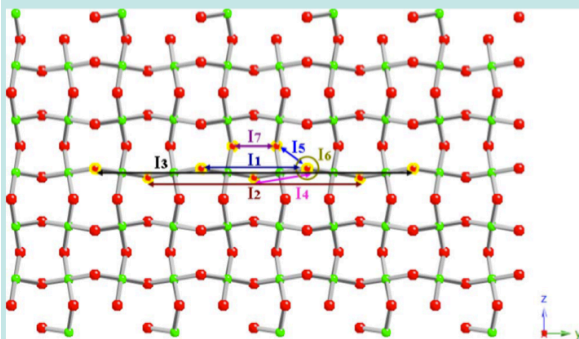
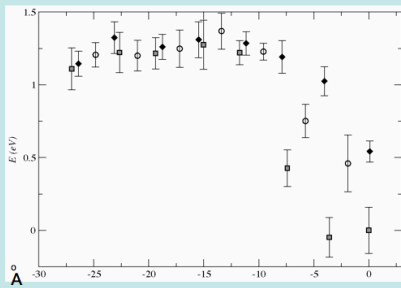


walls are elastically (a bit) softer

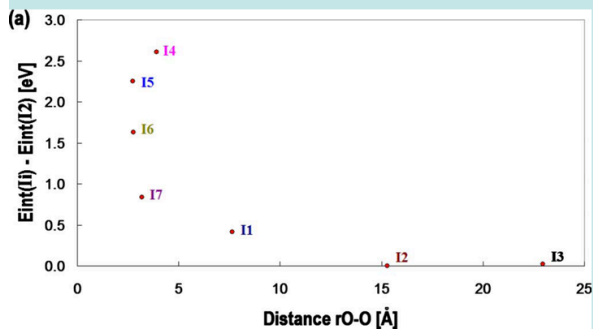


Relative change of the crystal total energy due to a single oxygen vacancy.

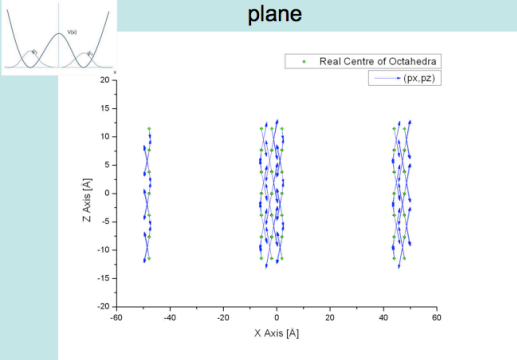
A twin wall along (100) with vanishing primary order parameter is at the origin. Circles denote vacancies for oxygen bridging Ti along [100], squares along [010] and diamonds along [001].



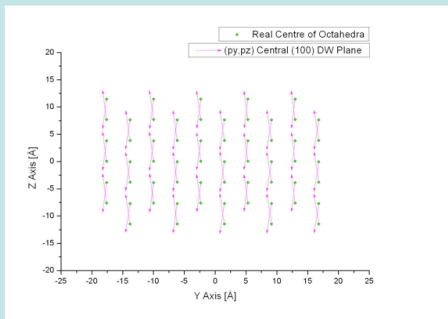
Correlation energy between vacancies are positive >> no clustering



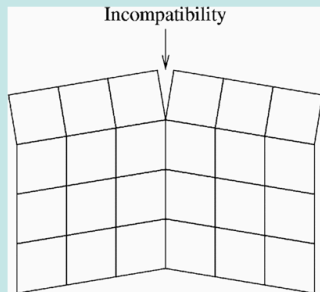
CaTiO₃: anti-ferroelectric Ti distortion in the x-z plane



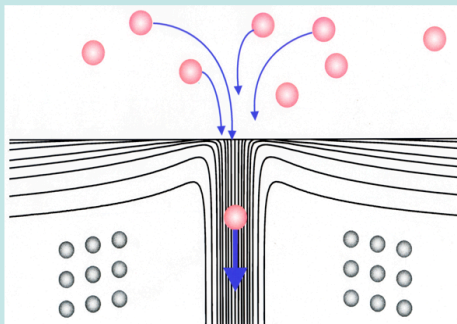
CaTiO₃ ferroelectric and anti-ferroelectric distortion in ferroelastic twin walls



Surface structure often result from the incompatibility between bulk microstructures and surface relaxations (thin films)

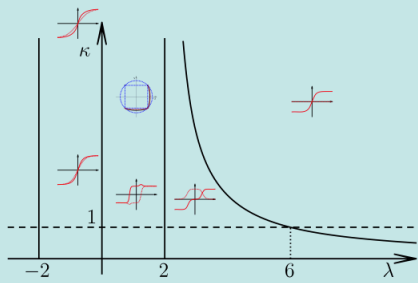


complex minimizer with 3 competing length scales: w , the surface relaxation and the exponential decay of the surface wave



Salje and Conti, Novak and Salje, Conti et al (2010)

phase diagram for bi-quadratic coupling

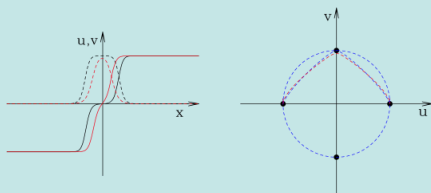


$$F_\lambda(u, v) = (1-u^2)^2 + (1-v^2)^2 + \lambda u^2 v^2 - c_\lambda$$

$$E_{\kappa, \lambda}[u, v] = \int F_\lambda(u, v) + |u'|^2 + \kappa |v'|^2 dx$$

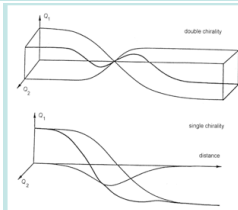
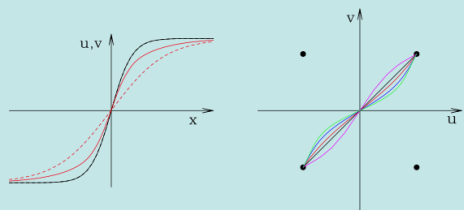
26

one kink (u) and one breather (v)



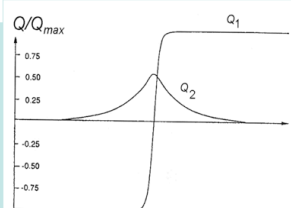
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two breathers can increase the gradient in photovoltaics



Two coupled order parameters

$$G = \frac{1}{2} A_1 Q_1^2 + \frac{1}{4} B_1 Q_1^4 + \frac{1}{2} g_1 (Q_1')^2 + \frac{1}{2} A_2 Q_2^2 + \frac{1}{4} B_2 Q_2^4 + \frac{1}{2} g_2 (Q_2')^2 + \lambda Q_1^2 Q_2^2$$



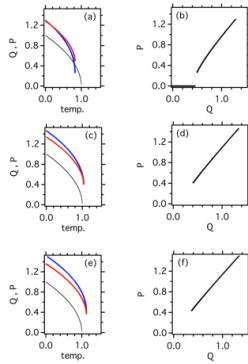
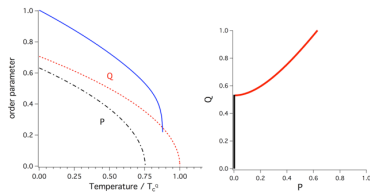
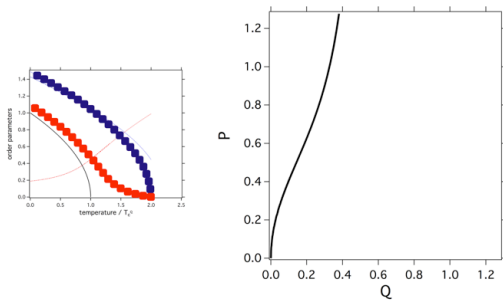
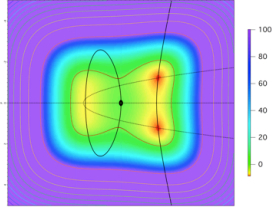
Linear-quadratic coupling

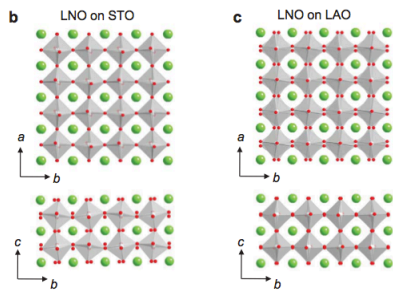
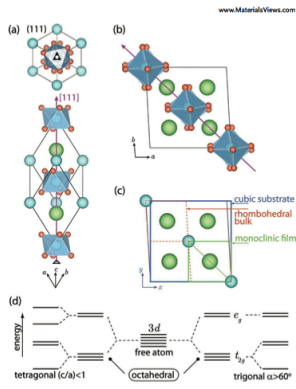
$$G(Q,P) = \frac{1}{2}aQ^2 + \frac{1}{4}Q^4 + \frac{1}{2}cP^2 + \frac{1}{4}P^4 + \frac{1}{2}\lambda QP^2.$$

$$F^Q = -2a/\lambda Q - 2/\lambda Q^3$$

$$F^P = -c - \lambda Q$$

$$Q^3 + (\lambda^2/2 + a)Q + c\lambda/2 = 0$$



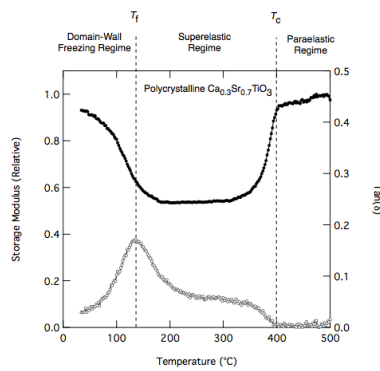


the next challenge: domain boundary engineering in thin films (here LiNiO_3 on SrTiO_3 and LaAlO_3)

dynamics of walls

ballistic (viscous),
accelerated,
jerky (avalanches)

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viscous motion:

extension of the Euler-Lagrange equation in d dimensions
using Landau-Khalatnikov

$$\left\{ \frac{\partial^2}{\partial t^2} + (d-1)r \frac{\partial}{\partial r} - \tau/g \frac{\partial}{\partial t} \right\} Q = \left\{ \frac{\partial}{\partial Q} \right\} G(Q)/g$$

same profile, also in the ballistic limit with $\partial^2/\partial t^2$

leading to Lorentz contraction, for $C=0$

$$Q(r,t) = Q_0 \tanh\left\{ \frac{(r-vt)}{w[1-v^2/c^2]^{1/2}} \right\}$$

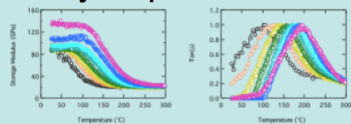
the wall profile does not change, only the wall thickness
contracts

Pinning potential can be simulated atomistically and lead to
very small pinning for thick walls ($w > 2$ unit cells)

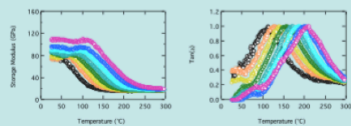
38

Frequency-dependence

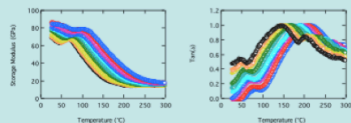
90:100 mN



200:220 mN



450:500 mN



Elastic response function

- $J(t) = \epsilon(t)/\sigma = J_{\text{unrelaxed}} + \Delta J(1 - \exp(-t/\tau))$

$$J(\omega) = J_{\text{unrelaxed}} + \Delta J / (1 + i\omega\tau) \quad \text{Debye}$$

- Extended Debye

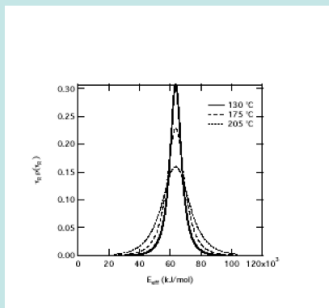
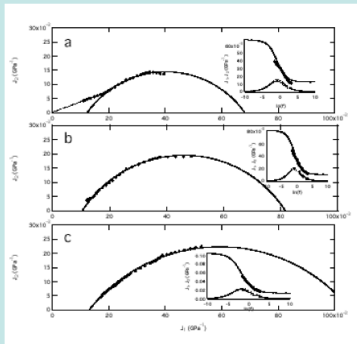
$$J(\omega) = J_{\text{unrelaxed}} + \Delta J / (1 + i\omega\tau)^\mu$$

- Equivalent to density function in τ

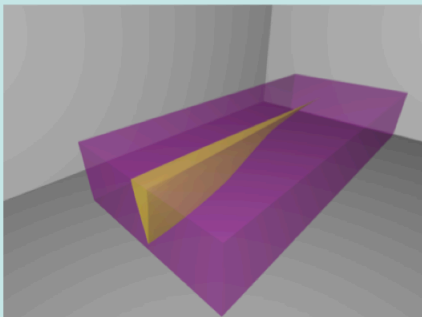
$$\rho(\tau) = (\tau^{\mu-1} \sin(\mu\pi) / \pi) / (1 + \tau^{2\mu} + 2\tau^\mu \cos(\pi\mu))$$

- First moment $\tau\rho(\tau)$ gives the probability function of τ

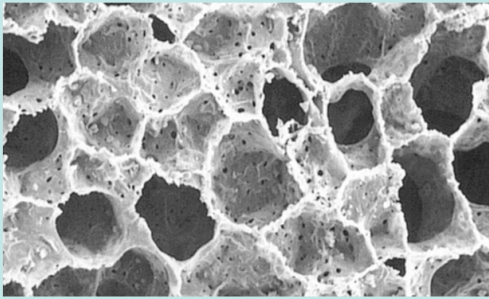
Elastic Cole-Cole plots: 'flattened' semicircles



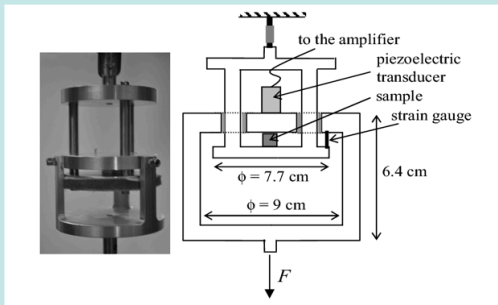
jerky movement: the noise of the propagating wall



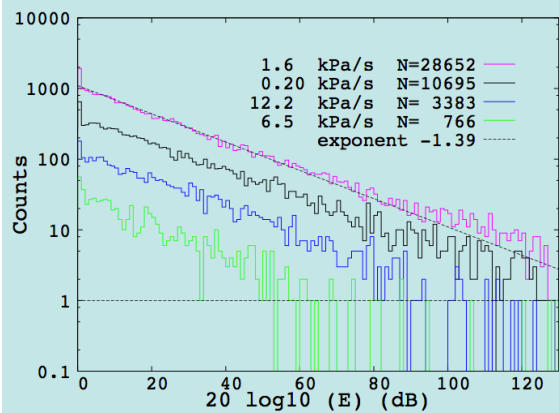
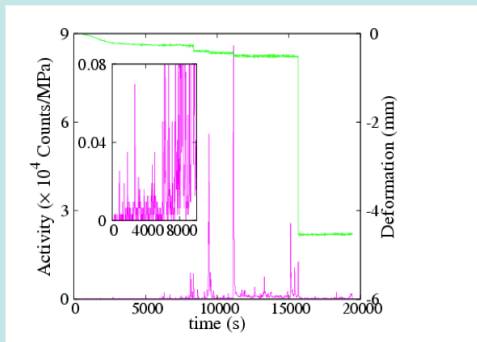
crumbling porous materials
fractal, also in magnetism



uniaxial stress

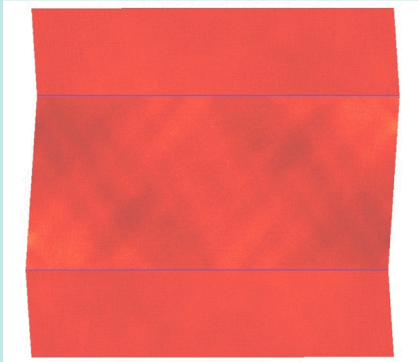
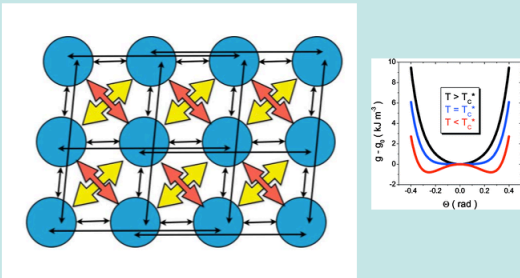


noise pattern



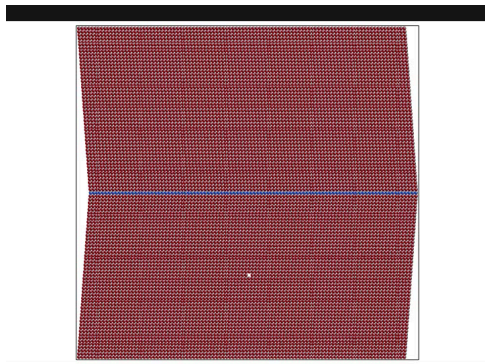
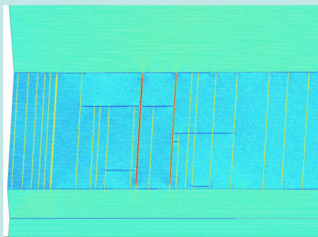
computer simulation: do jerks need defects? or can crystals crumble under elastic forces without being elastically unstable?

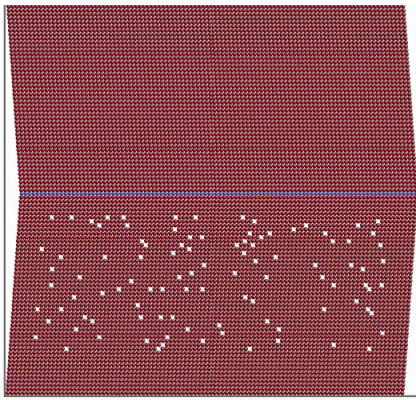
- the model: red and yellow lines are Landau springs



a defect free sample is sheared and jams via twin boundaries

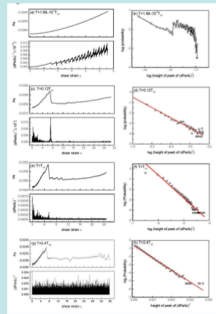
- notice the interplay between horizontal and vertical twin boundaries (Salje et al. PRB submitted)





the response is sawtooth, the statistics is Vogel-Fulcher or power law

- high temperature lead
- to exponential decays with
- VF law while low temperatures
- leads to a-thermal power law



Inverse activation energy leads to VF law (regime III) with 'phase transition' to a power law regime (II) at the VF temperature. Regime (I) shows a purely mechanical response.

